



AS2070: Aerospace Structural Mechanics

Module 1: Elastic Stability

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Dept. of Aerospace Engg., IIT Madras, Chennai

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BUCKLING OF BARS, PLATES, AND SHELLS

Don O. Brush
Bo O. Almroth



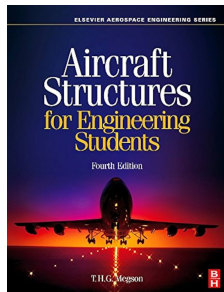
*Chapters 1-3 in Brush
and Almroth (1975).*

1 Introduction

- Elastic Stability
- Bifurcation
- Modes of Stability Loss

2 Euler Buckling of Columns

- Equilibrium Equations
- Kinematic Description
- The Linear Buckling Problem
 - The Pinned-Pinned Beam

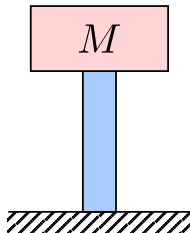


*Chapters 7-9
in Megson (2013)*

1. Introduction

Structural Stability: What?

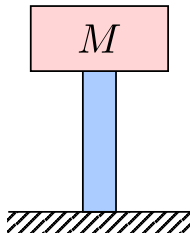
- Consider supporting a mass M on the top of a rod.



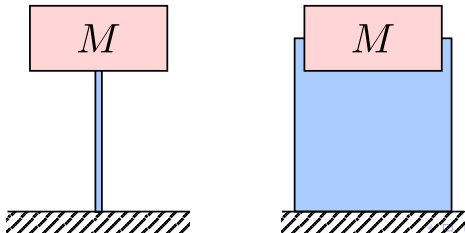
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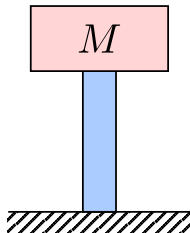
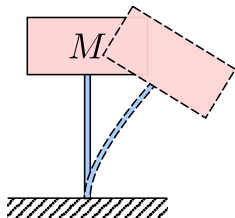
Two Extreme Cases:



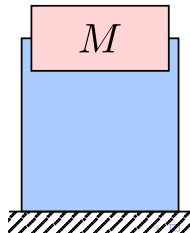
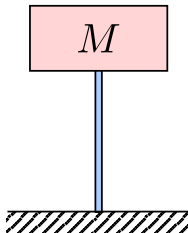
1. Introduction

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- Consider supporting a mass M on the top of a rod.
- Collapse is imminent on at least one!



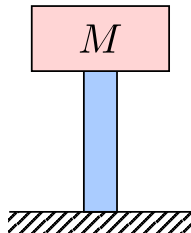
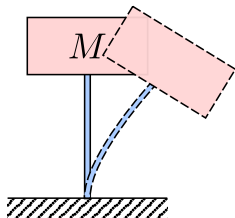
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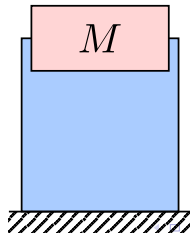
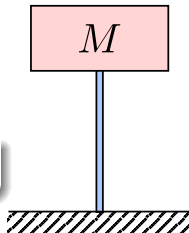
1. Introduction

Structural Stability: What?

- Consider supporting a mass M on the top of a rod.
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Two Extreme Cases:



How can we mathematically describe this?

1. Introduction

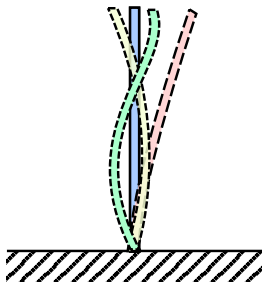
Structural Stability: Perturbation Behavior

Perturbation Behavior

Key insight we will invoke is behavior under **perturbation**:

How would the system respond if I slightly perturb it?

- Mathematically, by perturbation we mean *any change to the system's configuration*.
- In this case, this could be different deflection shapes.



1. Introduction

Structural Stability: Perturbation Behavior

Perturbation Behavior

Key insight we will invoke is behavior under **perturbation**:

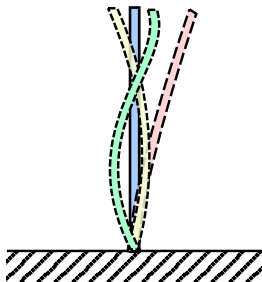
How would the system respond if I slightly perturb it?

- Mathematically, by perturbation we mean *any change to the system's configuration*.
- In this case, this could be different deflection shapes.

Question (Slightly more specific)

What will the system tend to do if an arbitrarily small magnitude of perturbation is introduced?

- Will it tend to **return to its original configuration**?
- Will it **blow up**?
- Will it do **something else entirely**?



1.1. Elastic Stability

Introduction

What do these words mean?

Elastic \rightarrow Reversible \rightarrow Conservative

Conservative System

- The restoring force of a conservative system can be written using a gradient of a **potential function**:

$$\underline{F} = -\nabla U.$$

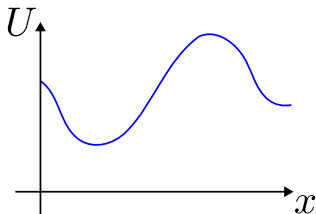
Equilibrium

- System achieves equilibrium when $\underline{F} = \underline{0}$, i.e.,

$$\nabla U = 0.$$

1D Example

Consider a system whose configuration is expressed by the scalar x and the potential is as shown.



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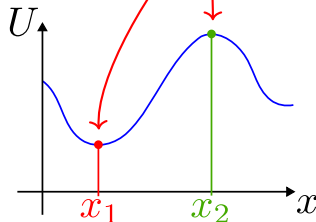
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1D Example

Consider a system whose potential is as shown. These are the equilibria.



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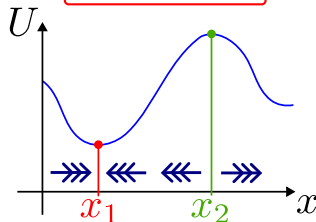
$$\nabla U = 0.$$

1D Example

Consider a system whose configuration is expressed by the scalar x and the potential is

Remember,

$$F = -\frac{dU}{dx}.$$



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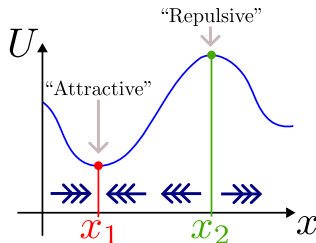
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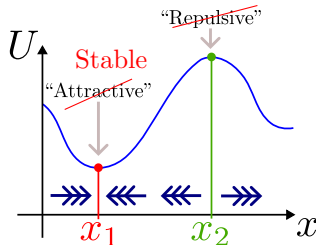
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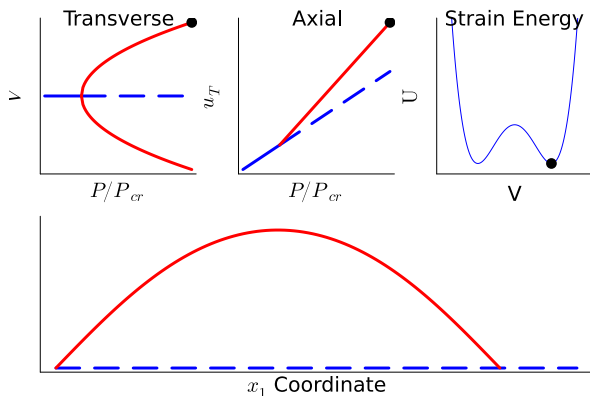
Consider a system whose configuration is expressed by the scalar x and the potential is as shown. **Unstable**



1.2. Bifurcation

Introduction

A system is said to have **undergone a bifurcation** if its state of stability has changed due to the variation of some parameter.

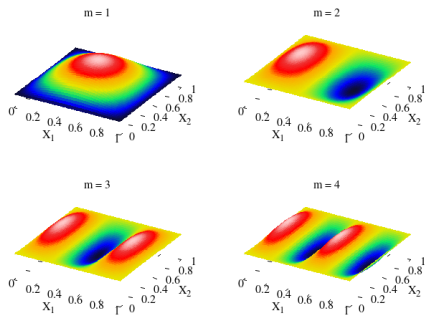


Example: A pinned-pinned beam undergoing axial loading.

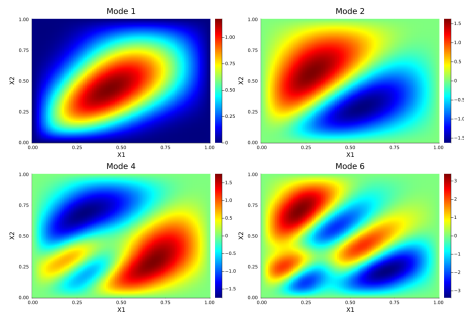
1.3. Modes of Stability Loss

Introduction

The **configuration** that a system can assume as it undergoes a bifurcation is the *mode* of the stability loss.



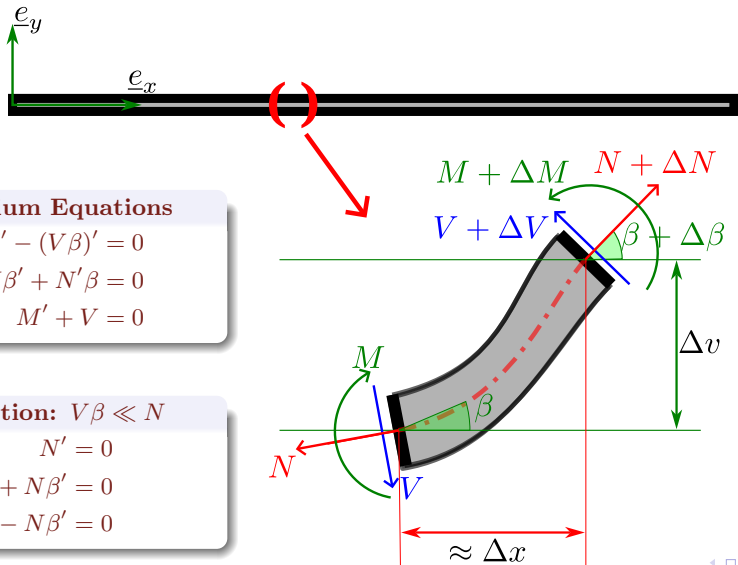
Example: Thin plate (pinned) under axial loading



Example: Thin plate (pinned) under shear loading

2.1. Equilibrium Equations

Euler Buckling of Columns



Equilibrium Equations

$$N' - (V\beta)' = 0$$

$$V' + N\beta' + N'\beta = 0$$

$$M' + V = 0$$

Assumption: $V\beta \ll N$

$$N' = 0$$

$$V' + N\beta' = 0$$

$$M'' - N\beta'' = 0$$

2.2. Kinematic Description

Euler Buckling of Columns



Displacement, Strain Field

$$u_x = u(x) - yv'(x)$$

$$u_y = v(x)$$

$$\varepsilon_{xx} = u'(x) - yv''(x)$$

Assumptions (E.B.T.)

Plane sections remain planar

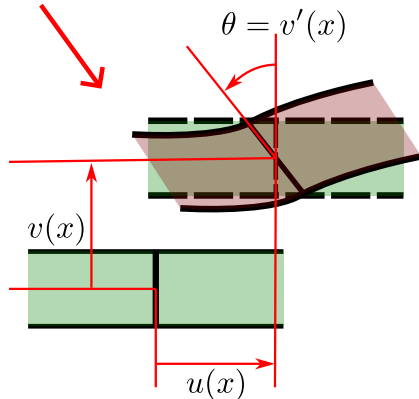
$$u, v \rightarrow u(x), v(x)$$

Neutral Axis remains \perp to sections

$$\beta \equiv \theta = v'(x)$$

Small displacements, rotations

$$\mathcal{O}(v^2, u^2, v'^2) \rightarrow 0$$



2.2. Kinematic Description

Euler Buckling of Columns



Displacement, Strain

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$$u_y = v(x)$$

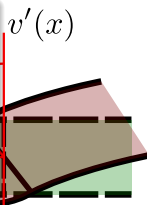
$$\varepsilon_{xx} = u'(x) - yv''(x)$$

Constitutive Modeling

$$\sigma_{xx} = E\varepsilon_{xx} = Eu' - yEv''$$

$$N = \int_{\mathcal{A}} \sigma_{xx} = EAu'$$

$$M = \int_{\mathcal{A}} -y\sigma_{xx} = EIV''$$



Assumptions

Plane sections remain plane

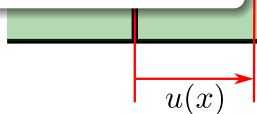
$u, v \rightarrow$ **Note:** y measured in Centroidal

Neutral Axis remains straight coordinates s.t. $\int_{\mathcal{A}} y = 0$.

$$\beta \equiv \theta = v'(x)$$

Small displacements, rotations

$$\mathcal{O}(v^2, u^2, v'^2) \rightarrow 0$$



2.3. The Linear Buckling Problem

Euler Buckling of Columns

- Substituting, we are left with,

$$N' = \boxed{EAu'' = 0}, \quad M'' - N\beta' = \boxed{EIv'''' - Nv'' = 0}.$$

Axial Problem

- Boundary conditions representing axial compression:

$$u(x=0) = 0, \quad EAu'(x=\ell) = -P$$

- Solution:

$$\boxed{u(x) = -\frac{P}{EA}x}$$

Transverse Problem

- Substituting $N = -P$ we have,

$$v'''' + k^2v'' = 0, \quad k^2 = \frac{P}{EI}.$$

- The general solution to this **Homogeneous ODE** are

$$\boxed{v(x) = A_0 + A_1x + A_2 \cos kx + A_3 \sin kx}$$

- Boundary conditions on the transverse displacement function $v(x)$ are necessary to fix A_0, A_1, A_2, A_3 .

2.3.1. The Pinned-Pinned Beam

The Linear Buckling Problem

- For a Pinned-pinned beam we have $v = 0$ on the ends and zero reaction moments at the supports:

$$\begin{aligned} v &= 0, & x &= \{0, \ell\} \\ v'' &= 0, & x &= \{0, \ell\} \end{aligned}$$

- So the general solution reduces to

$$v(x) = A_3 \sin kx,$$

with the boundary condition

$$A_3 \sin k\ell = 0.$$

- Apart from the trivial solution ($A_3 = 0$) we have

$$k_{(n)}\ell = n\pi \implies k_n = n\frac{\pi}{\ell}$$

or in terms of the compressive load P ,

$$P_{cr,n} = n^2 \frac{\pi^2 EI}{\ell^2}$$

- Interpretation:** If $P \neq P_{cr,n}$, $A_3 = 0$ to satisfy boundary conditions. But for $P = P_{cr,n}$, A_3 CAN BE ANYTHING!

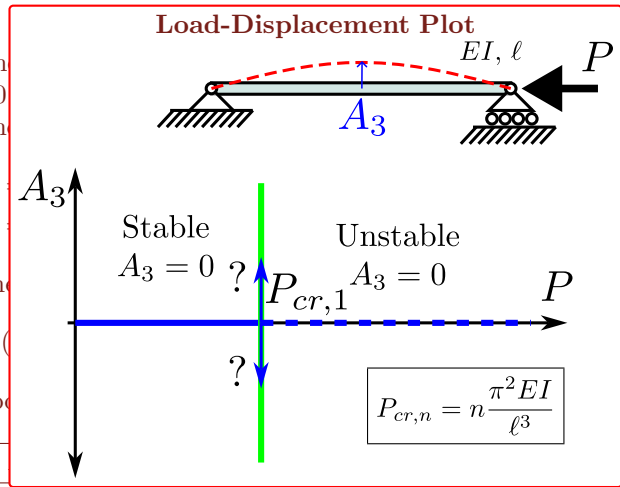
2.3.1. The Pinned-Pinned Beam

The Linear Buckling Problem

- For a Pinned-Pinned beam, we have $v = 0$ at both ends. The reaction moment is zero at both ends.

- So the general solution is $v(x) = A_1 \sin(\frac{\pi x}{\ell}) + A_2 \cos(\frac{\pi x}{\ell}) + A_3 x + A_4$

with the boundary conditions $v(0) = 0$ and $v(\ell) = 0$.



solution

$$n = n \frac{\pi}{\ell}$$

compressive

$$\frac{EI}{\ell^2}$$

$\neq P_{cr,n}$,

boundary

$$= P_{cr,n}, A_3$$

CAN BE ANYTHING!.

2.3.1. The Pinned-Pinned Beam: The Imperfect Case I

The Linear Buckling Problem

2.3.1. The Pinned-Pinned Beam: The Imperfect Case

The Linear Buckling Problem

References I

- [1] D. O. Brush and B. O. Almroth. **Buckling of Bars, Plates, and Shells**, McGraw-Hill, 1975. ISBN: 978-0-07-008593-0 (cit. on p. 2).
- [2] T. H. G. Megson. **Aircraft Structures for Engineering Students**, Elsevier, 2013. ISBN: 978-0-08-096905-3 (cit. on p. 2).

4. Class Discussions (Outside of Slides)

- Ball on a hill. 2D, 3D cases.
- Assumptions behind compression of a bar.